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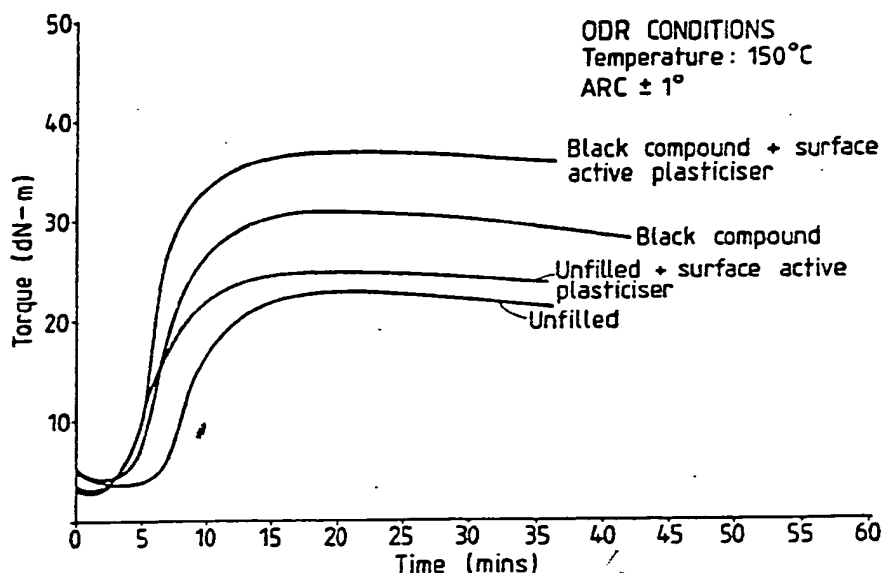
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(54) Title: A PROCESS FOR TREATING RUBBER

(57) Abstract

Classes of cationic surface active plasticiser accelerators (SAPA) with a multipurpose role which function as an internal processing agent at the lower conventional rubber processing temperature range of 30-100°C and then dissociate at the higher temperature used for vulcanisation (> 140°C) to form a secondary amine which functions as an organic accelerator of cure. Filler dispersion efficiency is enhanced by the presence of the surfactant and often vulcanisates have greater than normal strength. It is not necessary to include zinc oxide and stearic acid in the formulation to obtain a fast cure rate and excellent physical properties; however, the inclusion of some

zinc oxide is useful if scorch retardation is desirable and if vulcanisates with maximum heat ageing resistance are required. SAPA's can be used as accelerators of cure by themselves or in combination with conventional rubber accelerators. The particular classes used of SAPA are the fatty acid salts of alkyl alkylene diamine and alkyl imidazoline. SAPA may also comprise an alkyl bis alkylamide or a fatty acid salt of an alkyl alkane diamine. It is usually not necessary to use mould release agents as SAPA vulcanisates are self releasing due to the release, in situ, of a fatty acid component during cure.



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A PROCESS FOR TREATING RUBBER

This invention relates to a process for treating rubber utilising certain classes of cationic surfactants in the form of surface active plasticiser accelerators (hereinafter referred to as SAPA).

To enable rubbers to be processed it is customary to intimately mix into them liquids and low melting solids which function as internal lubricants or plasticisers during processing causing a reduction in viscosity, easing filler incorporation and reducing the frictional heat generated during the high shear rate processing operations of internal mixing, extruding etc. These plasticisers are considered to function in a physical rather than chemical manner and their function is not usually dependent on the temperature of mixing or curing. Usually their relative compatibility with a particular rubber is considered important and the solubility parameter concept is frequently used to predict compatibility, on the basis of a rubber and plasticiser possessing approximately similar solubility parameters being more likely to be compatible than the reverse situation. Compatibility of a plasticiser with rubber must be considered a concept or combination of properties, rather than a specific individual property and is assessed as follows.

Processing of Unvulcanised Rubber

1. The plasticiser's effect is measured by the rate at which it can be assimilated into the rubber during mixing and by the subsequent temperature generated and heat history of the mix.
2. The quantity of plasticiser able to be assimilated by the rubber without subsequent blooming and exudation of surface liquid is important together with the effect of plasticiser proportions on viscosity of the rubber mix.
3. Influence of a plasticiser on cure rate and state is also important and, as a generalisation, cure retardation is regarded as undesirable leading to loss of properties and greater costs.
4. The effect on dielectric properties of a rubber by a plasticiser can also be important.

Properties of Vulcanised Rubber

As a generalisation, at present, with the exception of polymerisable and crosslinkable plasticisers, such as acrylics and phenolics, the presence of a plasticiser in a rubber reduces the strength of its vulcanisate to a greater or lesser degree. Hence the relative effect of different plasticisers on strength reduction in a rubber mix is commonly used to assess its compatibility or efficiency. Sometimes, due to the lack of sensitivity of the rubber test techniques, changes in strength properties due to the presence of a plasticiser cannot be measured. Other properties often used to assess plasticiser compatibility and effectiveness are:- staining, colour stability, ageing resistance, volatility from the rubber during processing, curing and service; fluid extractability and retention of flexibility at low temperatures. This investigation concerns the effect of a cationic surfactant as a rubber compounding ingredient.

Cationic surfactants comprising the fatty acid salts of primary amines have been mixed with rubber in an attempt to improve flow characteristics, and the release and strength properties of rubber. However, the use of these primary amines has proved unsatisfactory for a number of reasons including scorching where the scorch properties of the rubber are very poor.

According to one aspect of the present invention there is provided a process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising a fatty acid salt of an alkyl alkylene diamine.

According to another aspect of the present invention there is provided a process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising a fatty acid salt of an alkyl alkane diamine.

According to yet another aspect of the present invention there is provided a process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising a fatty acid salt of an alkyl imidazoline. Preferably, the fatty acid salt of an alkyl imidazoline is selected from one of 1(2-hydroxyethyl)-2-heptadecenyl [2] imidazoline and 1 hydroxyethyl 2 oleyl imidazoline.

According to a further aspect of the present invention the use of a cationic surfactant comprising a fatty acid salt of an alkyl alkylene diamine in the treatment of rubber wherein the cationic surfactant is mixed with the rubber to provide a rubber compound with improved flow characteristics and release properties.

5 According to yet a further aspect of the present invention there is provided the use of cationic surfactant comprising a fatty acid salt of an alkyl alkane diamine in the treatment of rubber wherein the cationic surfactant is mixed with the rubber to provide a rubber compound with improved flow characteristics and release properties.

10 According to an additional aspect of the present invention there is provided a process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant, comprising an alkyl bis alkylamide.

15 According to yet another aspect of the present invention there is provided the use of a cationic surfactant comprising an alkyl bis alkylamide in the treatment of rubber wherein the cationic surfactant is mixed with the rubber to provide a rubber compound with improved flow characteristics and release properties. Conveniently, the cationic surfactant is used as a
20 dispersing and wetting agent for filler in rubber.

Preferably, in one process of treating rubber the fatty acid salt is used in the presence of a metal oxide retardant. Alternatively, the fatty acid salt of an alkyl imidazoline is used in the presence of a metal oxide retardant. Conveniently, the metal oxide retardant is selected from the
25 group comprising zinc oxide and lead oxide.

The fatty acid salt is preferably selected from the group comprising lauric acid; palmitic acid; soya acid; hydrogenated tallow acid; N-coco-1, 3-diamino-propane; N-tallow-1, 3-diamino-propane; N-oleyl-1, 3-diamino-propane; N-tallow-1, 3-diamino-propane di-oleate; N, stearic-1, 3-diamino-propane distearate; N-oleyl-1, 3-diamino-propane dioleate, and alkyl propylene
30 diamine.

Preferably, the alkyl bis alkylamide is selected from the group comprising N,N'-ethylene bis lauramide; N,N'-ethylene bis stearamide; N,N'-ethylene bis myristamide; N,N'-ethylene bis oleamide; N,N'-ethylene bis erucamide; and N,N'-ethylene bis behenamide.

5 In the process of treating rubber the mixture of rubber and cationic surfactant is vulcanised by heating in the presence of sulphur or a sulphur donating compound.

Embodiments of the present invention will now be described by way of example with reference to the accompanying drawings, in which:-

10 Figure 1 is a graph illustrating the curing properties achieved by the use of SAPA in natural rubber (NR).

Figure 2 is a graph illustrating the curing properties achieved by the use of SAPA in styrene butadiene rubber (SBR),

Figure 3 is a graph illustrating the curing properties of
15 polychloroprene rubber (CR) with SAPA,

Figure 4 is a graph illustrating the curing properties of Nitrile rubber with SAPA,

Figure 5 is a graph illustrating the comparative cure properties of SAPA with various rubber processing oils and processing additives,

20 Figure 6 is a graph illustrating the shear stress/shear rate properties of tread rubber with processing oils and SAPA,

Figure 7 (a) and 7 (b) illustrate the use of SAPA as a processing aid in both black and silica filled mixes,

Figure 8 (a) and 8 (b) illustrate SEM micrographs which demonstrate
25 the ability of the SAPA surfactant as a filler dispersion and wetting agent in natural rubber, and

Figure 9 (a) and 9 (b) illustrate SEM micrographs which demonstrate the ability of the SAPA surfactant as a wetting agent in SBR.

A number of experiments illustrating the improved properties of a
30 rubber achieved using SAPA are described below. The rubber prepared in each case is generally banded on a rubber mixing two roll mill in the conventional temperature range 30° to 100°C, but more usually at approximately 50°C. The SAPA and other small chemical compounds together with 1/3 of the filler content are then added to the rubber and dispersed. The remaining filler and
35 any other processing oil, if any, are then added and also dispersed. The step is followed by the addition and dispersion of sulphur.

Finally the mix is refined at least six times. During the treatment of the rubber SAPA dissociates at higher temperatures used for vulcanisation, that is greater than 140°C, to form, for example, a secondary amine, which
40 functions as an organic accelerator of cure.

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Test methods are conventional, as far as possible, and based on BS, ASTM or ISO rubber test method procedures. The mixing procedure used are as follows:-

1. Mill rolls set to approximately $50 \pm 5^{\circ}\text{C}$ and friction ration of 1.1:1.
- 10 2. NR banded around rolls and masticated to form a smooth coherent band.
3. Zinc oxide, stearic acid, CBS, Permanax BL were added with half the carbon black and incorporated into the rubber.
4. Remainder of carbon black was added together with the high strength plasticiser and dispersed.
- 15 5. Sulphur was added.
6. Mix was refined six times through a tight nip and sheeted off at 3 mm thickness for preparation of test specimens.

Series 1 Experiments

During an investigation of the properties of various processing aids
20 and plasticisers in particulate filler and fibre reinforced rubbers, it was observed that one class of liquids behaved unconventionally by, in certain instances, increasing both the Mooney viscosity and strength properties of unfilled (gum) and filled natural rubber. The particular experiment and series of compounds which this observation was made is detailed in Table 1
25 below, see Formulation 9.

Table 1 (a) Formulation used and properties of Gum (Unfilled) Vulcanisates Containing Different Types of Bonding Agents

Formulation	MIX NO.								
	1	2	3	4	5	6	7	8	9
pphr	100	100	100	100	100	100	100	100	100
NR (SMR 5)	100	100	100	100	100	100	100	100	100
Zinc oxide	5	5	5	5	5	5	5	5	5
Stearic acid	2	2	2	2	2	2	2	2	2
Sulphur	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
CBS	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Permanax EL	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
Ochedur RS	-	3.5	3.5	3.5	-	-	-	-	-
HMT	-	1.8	1.8	-	-	-	-	-	-
Vulkasil S	-	-	15	-	-	-	-	-	-
Ochedur A	-	-	-	2.5	-	-	-	-	-
Ochedur RL	-	-	-	-	5.5	-	-	-	-
Resimene 3520	-	-	-	-	-	2	-	-	-
Si69	-	-	-	-	-	-	2	-	-
Silane Z6052	-	-	-	-	-	-	-	2	-
*SAPA	-	-	-	-	-	-	-	-	2
Properties	1	2	3	4	5	6	7	8	9
Scorch time t_s at 150°C (mins) ²	7.0	3.5	7.0	7.0	8.5	7.0	7.5	3.5	3.5
Cure time (T_{95}) at 150°C (mins)	15.0	17.0	21.0	26.5	28.0	20.0	19.0	21.0	12.5
Maximum torque (dN-m)	22.5	26.5	33.5	23.0	23.5	26.0	24.0	13.0	14.5
Cure rate (dN.m/ min) (slope of steep region)	4.5	4.25	4.0	1.7	3.0	3.0	3.5	1.0	4.25

*SAPA is the surface active plasticiser

Table 1 (a) continued overleaf

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Table 1 (a) Continued.

Properties cont...	1	2	3	4	5	6	7	8	9
Tensile strength (MPa)	19.6	16.0	20.8	17.3	19.3	24.2	22.9	13.8	28.4
Elongation at break (%)	775	575	625	725	725	675	725	675	690
Tensile product (MPa x %) x 10 ⁻²	152	92	130	125	140	163	166	93	196
Modulus at 100% (MPa)	0.82	1.02	1.38	0.82	0.86	1.08	0.81	0.83	1.1
Tear strength (KNm ⁻¹)	49.8	37.5	41.0	56.3	42.2	54.9	45.7	47.3	54.6
Hardness (IRHD)	35	40	46	36	36	40	36	36	41
Compression set @ 100°C for 24 hrs (%)	45.2	39.1	36.4	36.4	42.0	52.2	38.9	34.7	41.6
$V_r \left(\frac{1}{V_1} \frac{V - V_1}{E} \right)$	0.7354	0.7122	0.7018	0.7523	0.7462	0.7277	0.7310	0.7395	0.7115
<u>Aged properties</u> (70°C for 1 week)									
Tensile strength (MPa)	12.6	13.8	13.6	13.4	15.2	15.8	1.9	2.2	16.0
Retention, %	64.3	86.3	65.4	77.5	78.8	65.3	8.3	15.9	66.1
Elongation at break (%)	650	450	475	550	635	635	220	315	536
Retention, %	83.8	72.2	76	75.6	87.6	79.3	30	47	77.5
Hardness (IRHD)	43	44	50	39	38	44	41	40	46
Increment	8	4	4	3	2	4	5	4	5

*SAPA in the surface active plasticiser

Table 1 (b) Formulation Used and Properties of Black Vulcanisates Containing Different types of Bonding Agents

Formulation	Mix No.								
pphr	1	2	3	4	5	6	7	8	9
NR (SMR 5)	100	100	100	100	100	100	100	100	100
Zinc oxide	5	5	5	5	5	5	5	5	5
Stearic acid	2	2	2	2	2	2	2	2	2
Sulphur	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5
CBS	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Permerax BL	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
Carbon Black (HAF N330)	30	30	30	30	30	30	30	30	30
Ochedur RS	-	3.5	3.5	3.5	-	-	-	-	-
HMT	-	1.8	1.8	-	-	-	-	-	-
Vulkasil S	-	-	15	-	-	-	-	-	-
Ochedur A	-	-	-	2.5	-	-	-	-	-
Ochedur RL	-	-	-	-	5.5	-	-	-	-
Resimene 3520	-	-	-	-	-	2.0	-	-	-
Si69	-	-	-	-	-	-	2.0	-	-
Silane Z6062	-	-	-	-	-	-	-	2.0	-
SAPA*	-	-	-	-	-	-	-	-	2.0
Properties	1	2	3	4	5	6	7	8	9
Scorch time t_s at 150°C (mins) ²	4.8	2.5	3.5	4.0	6.0	4.8	5.8	2.0	3.0
Cure time (T_{95}) at 150°C (mins)	14	15	22	28	28	21	19	13	13
Maximum torque (dN-m)	31	43	49	39	37	37	33	34	37

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Table 1 (b) Continued

Properties cont..	1	2	3	4	5	6	7	8	9
Cure rate (dNm/ min) (slope of steep region)	5.5	8.5	5.5	2.5	3.5	4.8	4.0	5.5	6.0
Tensile strength (MPa)	26.1	21.4	19.8	17.3	15.8	26.8	23.8	25.6	30.4
Elongation at break (%)	600	425	425	460	525	590	620	575	600
Tensile product (MPa x %) x 10 ⁻²	157	91	84	80	83	158	179	147	182
Modulus at 100% (MPa)	2.0	4.0	3.9	3.0	2.6	2.5	2.3	2.2	2.4
Tear strength (KNm ⁻¹)	54.3	130.8	117.3	27.3	29.5	138	126.2	115	122
Hardness (IRHD)	54	72	77	72	72	64	60	55	62
Compression set @ 100°C for 24 hrs (%)	50	39.1	47.0	50.3	55.4	51.9	49.4	64.3	45.7
$V \left(\frac{1}{V_1} - \frac{V}{V_1} \right)$	0.6661	0.6191	0.6327	0.6795	0.6794	0.6640	0.6696	0.6705	0.6391
<u>Aged properties</u>									
(at 70°C for 1 week)									
Tensile strength (MPa)	25.9	19.1	12.9	13.5	14.3	21.7	16.9	18.9	22.0
Retention %	99	79.9	65.2	77.9	90.4	80.9	58.7	64.5	72.5
Elongation at break (%)	550	320	275	325	350	445	425	400	475
Retention %	91.7	75.3	64.9	70.7	66.7	75.4	68.5	69.6	79.2
Hardness (IRHD)	58	77	83	79	77	70	66	60	67
Increment	4	5	5	7	5	6	6	5	5

*SAPA is the surface active plasticiser

Series 2 ExperimentsSurface Active Plasticiser Accelerator in Natural Rubber

5 Following this observation another experiment was carried out in our laboratory to ascertain whether this apparent reinforcing effect would also apply to both unfilled NR (gum) and carbon black reinforced NR. The formulations used and results obtained are given in Table 2 below and Figure 1; the physical properties at two cure states were measured, namely t_{90} and $t_{95\%}$ cure.

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Table 2- Reinforcing Effect of Surface Active Plasticiser Accelerator
(SAPA no. 1) on Unfilled and Filled NR

	Controls		SAPA Plasticiser	
	Unfilled	Filled	Unfilled	Filled
Natural Rubber (SMR 5)	100	100	100	100
Zinc oxide	5	5	5	5
Stearic acid	2	2	2	2
HAF Black	-	30	-	30
Sulphur	2.5	2.5	2.5	2.5
CBS	0.5	0.5	0.5	0.5
Permanax BL	1.5	1.5	1.5	1.5
Surface Active Plasticiser Accelerator (1)	-	-	2	2

*(N330. Vulcan 3 of Cabot Carbon)

*(N330. Vulcan 3 of Cabot Carbon)								
properties	Unfilled (gum stock)				Carbon Black filled			
	Control		SAPApresent		Control		SAPApresent	
<u>Cure properties</u> ODR at 150°C	1 arc 3 arc		1 arc 3 arc		1 arc 3 arc		1 arc 3 arc	
Max torque (lb in)	22.5	49	24.5	57	31	63	37	75
Min torque (lb in)	18	45	21	55	26.5	60	34	70
t95 (m)	15	17	12.5	12	14	14	13	11
t2 (m)	7	8	3.5	4	3.5	5	3	3
Mooney Viscosity ML ₁₊₄ 100° C	16		18		27		28	
<u>Physical Properties</u> Cure Conditions	15 m at 150°C							
Tensile Strength MPa	17		21.2		25.6		26.2	
Elongation at break %	760		750		610		530	
300% modulus MPa	1.4		1.8		8.2		9.9	
Hardness IRHD	39		42		52		56	
<u>Cure Conditions</u>	20 m at 150°C							
Tensile Strength MPa	19.6		28.4		26.1		30.4	
Elongation at Break %	775		690		600		600	
300% modulus MPa	-		-		-		-	
Hardness IRHD	39		42		54		62	
Tear Strength kN/m ⁽ⁱ⁾	99		109		108		144(244)(ii)	
Compression set %	46		41		50		46	
24 hr. at 70°C								

(i) BS903. (ii) An occasional very high value was observed.

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Examination of these results show the following features:
the addition of SAPA:

- 5 i) Increases the cure state of both unfilled (47%) and filled (61%) NR and reduces the induction time (processing safety) before cure commences (see figure 1).
- ii) Increases the strength properties significantly, i.e. UTS increases by 45% and 16% in unfilled and filled vulcanisates respectively and the comparative tear strength increases are 10% and 33%.
- 10 iii) Hardness increases significantly by 17% in unfilled and 15% in filled vulcanisates.
- iv) Compression set reduces by 12% in unfilled and 8.5% in filled vulcanisates.
- 15 v) Most unexpectedly and inexplicably the addition of the liquid SAPA increases Mooney Viscosity by small but significant amounts with the increase being 12.5% in unfilled and 4% in filled mixes.

During the Series 1 and Series 2 experiments the unvulcanised rubbers were observed to possess outstandingly good flow and processing properties and
20 these characteristics were now observed in more detail.

Series 3 Experiments

Examination of SAPA in some Synthetic Rubbers

25

SAPA was examined in some common synthetic rubbers for its effect on processing and properties and the results are now systematically given and commented upon.

SBR Rubber

30 This rubber was examined in the filler reinforced condition, as in the unfilled condition it has only very poor strength; both carbon black and precipitated silica reinforced rubbers were investigated. Results are given in Table 3 below and Figure 2.

Table 3 - SBR Rubber. SAPA compared with Aromatic Oil and Triethanolamine.

	Carbon Black Reinforced			Silica Reinforced	
	No plasticiser	Aromatic Oil	SAPA	Treithanolamine	SAPA
Intol 1502	100	100	100	100	100
ZnO	5	5	5	5	5
Stearic acid	1	1	1	1	1
HAF Black	30	30	30	-	-
MBT	1.5	1.5	1.5	1.5	1.5
DPG	0.5	0.5	0.5	0.5	0.5
Sulphur	2.0	2.0	2.0	2.0	2.0
Permanax B	1.0	1.0	1.0	1.0	1.0
Ultrasil VN3	-	-	-	40.0	40.0
Dutrex 729	-	2.0	-	-	2.0
SAPA	-	-	2.0	-	2.0
Triethanolamine	-	-	-	2.0	-
Mooney Viscosity ML1+4 at 100°C	50	47	44	72	64
Cure Conditions	30	minutes		at	150°C
Tensile Strength MPa	12.1	11.6	12.2	9.3	14.0
Tensile strength after 7 days at 70°C	11	9.4	10	7.6	9.0
EB %	420	400	410	460	640
EB % after 7 days at 70°C	390	380	380	370	520
Hardness IRHD	60	60	60	70	71
Hardness after 7 days at 70°C	60	59	61	71	71
Tear strength N / 2mm	80	150	73	90	106
Compression set after 48 hr / 70°C	13	12	10	10	20

Continued

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Table 3 - Continued

Processing Properties	Carbon Black Reinforced			Silica Reinforced	
	No plasticiser	Aromatic oil	SAPA	Triethanolamine	SAPA
Flow	Poor surface finish on compression moulded sheet; stress lines and small depressions present	Intermediate dull finish flow lines visible	Glossy finish with no faults present. Stress free moulding	Poor surface finish; sheet was buckled and distorted due to moulding stresses	Glossy surface finish with no surface defects or stresses in sheet
Mould Release properties	Mould release essential	Mould release desirable	No mould release needed	Mould release is a major problem	Mould release excellent

Processing and Curing Properties

The behaviour of SAPA in SER is different from its response in NR as can be seen by the following interpretation of the data in Table 3 and Figure 2. In SER the plasticiser SAPA behaves conventionally as its inclusion lowers the _____

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Mooney viscosity, whereas in NR the Mooney viscosity was increased indicating some chemical response was occurring; in carbon black rubbers the reduction in Mooney viscosity, for the addition of only a small amount (2phr) was 12% for SAPA compared with 6% with aromatic oil and in a silica filled rubber the viscosity reduction compared with triethanolamine was also considerable.

Moulding

The SBR mixes containing SAPA possessed markedly superior flow and processing properties to their controls by producing undistorted stress free test specimen sheets when compression moulded from a cold thick round blank (of 10mm thickness) by the simple application of pressure. The equivalent control rubber all gave moulded sheets possessing defects due to flow problems.

15

Physical properties of particular note, however, are the cure activation effect of SAPA in an all-silica filled rubber where it out-performs the standard activator triethanolamine; it should be noted that both SAPA and triethanolamine (TEA) in a silica filled SBR give the same state of cure, as determined by an oscillating disc rheometer (ODR). The inclusion of SAPA increases the tensile strength (50%), elongation at break (39%) and the tear strength (17%) over the conventional TEA containing silica SBR; compression set is inferior. SAPA gives about the same physical properties in a carbon black filled SBR as does a standard aromatic oil (see Table 3 and Figure 2) but gives substantially better release for metal surfaces.

Series 4 Experiments

Examination of SAPA in some Synthetic Rubbers

For this purpose rubbers were divided into two classes; strain crystallisable (CR) and non-strain crystallisable (NBR). The results are shown in Tables 4 and 5 and Figures 3 and 4 showing a comparison of SAPA effects versus conventional plasticisers as controls.

Table 4 - Polychloroprene. SAPA compared with Dioctylphthalate

	Unfilled (gum stock)		Carbon Black filled	
	Control	SAPA present	Control	SAPA present
Neoprene GRT	100	100	100	100
ZnO	5	5	5	5
Magnesia (MgO)	4	4	4	4
Robac 22	0.5	0.5	0.5	0.5
HAF Black	-	-	50	50
Permanax B	1	1	1	1
SAPA	-	2	-	2
DOP	-	-	2	-
Mooney Viscosity ML 1+4 at 100 C	30	29	15	16
Cure conditions	t _{95%}	by	ODR	- Figure 3
Tensile Strength MPa	6.4	9.9	19.7	19.8
Tensile Strength MPa After 7 days at 70°C	5.9	4.8	18.4	18.3
Elongation at break %	580	840	350	330
Elongation at break % After 7 days at 70°C	480	500	345	335
Hardness IRHD	42	45	80	81
Hardness IRHD After 7 days at 70°C	43	47	81	82
Tear Strength N	87	37.5	115	112
Compression set 48 hr at 70 C	20	22	9	12
<u>Processing Properties</u>	Poor flow and mill roll release. Difficult to mill and mould. Stress lines on cured mouldings.	Mill flow and roll release excellent. No stress lines or distortion of cured mouldings.	Mill flow difficult due to high black content. High shear heat generation during mixing. Distorted mouldings if blank preparation not	Easy processing rubber; low heat generation during mixing. Moulds readily with no flow or stress problems in final moulding.

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Table 5 - Nitrile Rubber. SAPA compared with Dioctylphthalate in a Carbon Black Reinforced Mix

	Control Ester plasticiser DOP	SAPA present
Breon 1042	100	100
ZnO	5	5
Stearic acid	1	1
CBS	1	1
TMT	0.5	0.5
Sulphur	1.5	1.5
Permanax B	1	1
HAF Black	30	30
DOP	2	-
SAPA	-	2
Mooney viscosity ML 1+4 at 100°C	53	52
Tensile Strength MPa	13.9	15.7
Tensile Strength MPa after 7 days at 70°C	13.5	11.4
Elongation at break %	390	400
Elongation at break after 7 days at 70°C	380	370
Hardness IRHD	69	65
Hardness after 7 days at 70°C	67	66
Tear strength N	92	68
Compression set 48h/70°C	21	6.5
Processing Properties	Distorted and stressed moulded sheet with poor surface finish.	Undistorted moulding with high gloss defect free surface.

Cure Conditions 15'/150°C

Polychloroprene and SAPA

The effect of SAPA on the Mooney viscosity of CR is similar to a conventional plasticiser in both unfilled and filled rubbers. Cure rate is not significantly affected by SAPA but the cure state (t_{95} Modulus) of the unfilled CR is considerably enhanced; the cure state of the filled CR is only marginally enhanced, possibly because insufficient SAPA has been added to the CR mix which contains 50 phr of HAF black for maximum tensile strength (the NR and SBR mixes only contained 30 phr of black). Processing of the SAPA containing rubbers is markedly improved by the presence of SAPA both during milling and moulding with mouldings possessing flaw free surfaces and being free of stress and distortion problems. Physical properties are not improved by the presence of SAPA in CR where its effect seems similar to that of a conventional plasticiser.

15 Nitrile Rubber and SAPA (Table 5 and Figure 4)

The effect of SAPA on the viscosity and cure properties of NBR is similar to that of a conventional ester plasticiser such as di-octyl phthalate (DOP). With the proportion of SAPA used in this comparison the effect on physical properties is increased as SAPA contradictorily given NBR a higher tensile strength but lower tear strength; an explanation of this may be seen by observing that the compression set of the SAPA/NBR is exceptionally low (6.5%) hence the SAPA/NBR may have a greater degree of cure and hence crosslinking than its DOP/NBR counterpart though this is not indicated by the ODR results of Figure 4 which show DOP and SAPA to give the NBR similar rates and states of cure. Processability of SAPA containing nitrile rubber was markedly superior to the DOP control.

Series 5 Experiments. SAPA as an accelerator of rubber vulcanisation

30 In all these investigations a common feature is the ability of the SAPA to act as a cure rate and cure state promoter and it was decided to examine its potential as a rubber accelerator. As a base compound for this investigation a typical NR/SBR truck tyre sidewall compound (see Table 6) was chosen in which to vary SAPA and the other ingredients of a conventional curing system.

Table 6 - Truck Tyre Compound used to examine the potential of SAPA as an accelerator.

	NR (SMR20)	30 pbw
5	SBR 1500	70
	FEF Carbon Black	51
	IPPD	2
	Microcrystalline WAX	3
	Zinc oxide	4
10	Stearic acid	2
	Santocure MOR	0.25
	CBS	0.25
	Sulphur	2
	Processing oil/additive	Variable

Comparison of SAPA with Common Rubber Processing Oils (Table 7)

It is noteworthy, from the data in Table 7, that the SAPA containing rubber (10 phr SAPA) has a higher strength than its hydrocarbon oil analogues; its strength is about the same as that of a non-oil containing mix, but, the SAPA mixes process and flows exceptionally easily.

Also, it is observed that the mix containing only SAPA has a very short scorch time, 3', at the relatively high level of 10 phr SAPA used and hence is acting as a cure rate accelerator to the extent of perhaps being able to induce scorch problems. This aspect of scorch control is now examined in detail as mixes with scorch times of 3' are not usually considered as practical for processing by the rubber industry's tyre manufacturers.

15 It was thought possible that SAPA was performing similarly to stearic acid but the data in Table 7 demonstrates that the modes of action of SAPA and stearic acid must be different.

Table 7 - Comparison of SAPA with Rubber Processing Oils/Additives

	No oil	Aromatic oil	Naphthenic oil	Stearic acid	Strucktol SWB 212	SAPA
Tensile strength MPa	19.3	17.9	16.4	19.5	19.5	19.5
% E.B.	580	660	660	580	570	595
300% modulus, MPa	8.4	6.5	5.7	8.6	8.7	8
Hardness IRHD	61	53	51	65	62	57
% Resilience	47	44	46	44	44	50
Tear strength N/2 mm sample	91	85	115	114	94	129
<u>Cure Properties</u>						
t ₉₀ at 160°C	16	20½	22	21½	20	7
Mooney viscosity 100°C	47	43	42	40	42	50
Mooney scorch ML 125°C	20 mins	24	19½	22½	24½	3
Banbury mixing time	13 mins	10	10	10	10	10
Dump temperature °C	135	115	115	124	126	120
Proportions of Processing aid in phr	0	10	10	10	10	10

Table 7 - (continued)

	Naphthenic oil (sun oil) Circosol 4240				Struktol Smb212	Stearic acid	5phr Iraqi oil + 5phr Struktol Smb212	5phr Iraqi oil + 5phr stearic acid	SAPA	5phr Iraqi oil + 5phr SAPA
	5phr	7.5phr	10phr	12.5phr	10phr	10phr	5 I. oil + 5 Smb 212	5phr I. oil + 5 phr stearic acid	10phr	
Tensile strength MN/m ²	18.9	18.5	16.4	16.7	19.5	19.5	18.7	18	19.5	17
100% modulus MPa	2.1	2	1.6	1.5	2.4	2.6	2.3	2	2.2	1.5
300% modulus MPa	7.6	7.3	5.7	5	8.7	8.6	8	7.4	8	5
Tear strength N/2mm thick sample	92	97.5	115	111	94	114	111	109	129	13
% Elongation at break	615	630	660	715	570	580	590	600	595	670
Hardness IRHD	56	55	51	50	62	65	58	56	57	56
Rebound resilience %	48	46	46	45	44	44	45	46	50	48
Optimum curing time (T ₉₀) at 160°C	18'30	17	22	25	20	21'30	20'30	21'30	7	7
Mooney viscosity ML 1+4 100°C	47	42	42	39	42	40	48	44	50	40
Mooney scorch ML 1+4 125°C	19'30	20'30	19'30	23'30	24'30	22'30	19	18'30	3	4
Mixing cycle, mins	10	10	10	11	10	10	10	10	10	10
Starting temperature °C	20	21	20	19	20	18	21	18	20	19
Cure temperature °C	122	117	115	117	126	124	114	112	120	117

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Elimination of the Cure Activation and Acceleration Systems

5 It was observed from the results of Table 7 that whilst the physical properties of SAPA containing rubber vulcanisates were better than its processing oil analogues by between 5-15% though similar to the flow additives Struktol SWB 212 and Stearic Acid, the scorch time of the SAPA mixes was short at the relatively high proportions (1 to 10) used, preferably 7.5p. Hence an investigation using the base compound of Table 6, was conducted to try and resolve this scorch problem; the method was to omit the zinc oxide/stearic acid activator and
10 accelerator system from the rubber formulation; initially some PVI (d) was retained to try and retard cure but this was found to be ineffective (see Table 8) and not required.

15 Table 8 - Elimination of the cure activator and accelerator systems from SAPA containing rubber formulations

Base mix, as shown in Table 6.

All mixes contained 2phr of sulphur (Banbury mixed)

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Mix No.	Reducing SAPA				
	1	2	3	4	5
No accelerator/ activator present in mix	7.5 phr SAPA Retarder FVI = 0.5 phr ZnO = 0 SA = 0 CBS = 0 MCR = 0	3 phr SAPA Retarder FVI = 0.5 phr ZnO = 0 SA = 0 CBS = 0 MCR = 0	2 phr SAPA Retarder FVI = 0.25 phr ZnO = 0 SA = 0 CBS = 0 MCR = 0	1.5 phr SAPA Retarder FVI = zero ZnO = 0 SA = 0 CBS = 0 MCR = 0	1 phr SAPA Retarder FVI=zero ZnO = 0 SA = 0 CBS = 0 MCR = 0
		<u>Cure Properties</u>			
Mooney Scorch at 125°C (t ₅) mins	7'30	13	12	12 '30	17
Mooney viscosity ML 1+4 100°C	38	41	44	44	46
Optimum curing time at 140°C mins	15'	21'50	23'	38	39'30
		<u>Physical Properties</u>			
Tensile strength MPa	15	16.5	15.5	15.9	15.3
100% modulus MPa	2.15	2.45	2.5	2.61	2.3
300% modulus MPa	7	8.5	8.5	9.2	8.3
Tear Strength N/2 mm	82	76	68	57	58
%Elongation at break	580	520	500	480	500
Hardness IRHD	55	59	59	61	60
Rebound resilience %	47	46	47	49	49

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The results of Table 8 show that relatively high SAPA proportions (e.g. 7.5p) give short scorch times (6-7 minutes) but by reducing the SAPA to 1-3 phr level increases the scorch time to 17-13 minutes, usually considered industrially acceptable. Also, using SAPA, it is possible to eliminate the conventional cure activation system (ZnO and Stearic Acid) and the delayed action accelerators (CBS and Santocure MOR) and, the prevulcanisation inhibitor PVI, whilst retaining the principal cross-linking agent, sulphur, at the modest proportion of 2 phr. Physical properties remain consistently good over the range of SAPA proportions used, 1-7 phr, with only a reduction in hardness becoming apparent at the higher (7.5 p) SAPA levels.

The processing and flow properties of all SAPA containing systems were found to be outstandingly good (see later).

15 This combination of cure activation and acceleration plus processability properties in a rubber mix is considered to be unique.

Series 6 Experiments. Zinc Oxide as a Scorch Control Additive in NR/SBR
20 Rubber Mixes Accelerated with SAPA (Table 9).

Table 9 demonstrates the effect of first introducing ZnO and then later stearic acid into a rubber mix containing only sulphur as a curative and from which the conventional accelerators have been omitted. It can be seen that when no ZnO and stearic acid is present a mix with 1.5 phr of SAPA has a scorch time of 15' and an optimum (t_{90}) cure time of 22'. Introducing 1 phr of ZnO increases the scorch time from 15' to 100' and the t_{90} cure time from 22' to 42'; further additions of ZnO (mixes A and B) and later stearic acid (mix B) have little to no effect on further extensions of scorch time or t_{90} curing time. The inclusion of the ZnO results in some reduction of tensile strength.

The use of stearic acid as part of the acitvator system does not seem to be necessary in the formulation.

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Table 9 - Zinc oxide as a scorch control additive in NR/SBR SARA rubber mixes

Base compound NR/SBR mix of Table 6 (2phr of sulphur - mill mixed)
(1.5 phr of SARA)

	A	B	C	D
Variable	NR/SBR Blend No accelerator	No accelerator	No accelerator	No accelerator
	Reducing	ZnO/Stearic	acid	No ZnO/Stearic acid
Property	ZnO = 4 phr Stearic acid = 2phr	ZnO = 2 phr Stearic acid = 1phr	ZnO = 1 phr Stearic acid = zero	
<u>Cure Properties</u>				
Mooney Scorch at 125°C, min.	110	100	100	15
Mooney viscosity ML 1+4 100°C	43	42	47	50
Optimum curing time at 160°C (T ₉₀)	41'30	40'	42'30	22
<u>Physical Properties</u>				
Tensile strength MPa	13.3	14.2	14.87	17
100% Modulus MPa	1.96	2.1	2.3	2.7
300% Modulus MPa	6	6.8	7.7	9.8
Tear strength N/ 2mm Thick sample	71.6	68.8	67	60
% Elongation at break	570	535	505	475
Hardness IRHD	56	54	57	57
Rebound	43.5	44	45	53
Resilience '%'. 				

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Zinc Oxide as Scorch Control Additive in NR mixes containing SAPA. (Table 10)

An investigation was conducted to ascertain whether the scorch retardation effect of ZnO, apparent in the NR/SBR blend, also applied to a single
5 polymer system, namely NR. The results are given in Table 10 for a carbon black reinforce formulation similar to that of Table 6 but based on only NR; the accelerators CBS and Santocure MOR were also present at 0.25/0.25 parts respectively (as in Table 6). It is seen that decreasing the ZnO content progressively from 4 part to 1 parts increases the scorch time in a regular
10 and uniform manner from 14' to 24' in mixes containing 0.5 p SAPA at higher SAPA levels, i.e. 1.5 parts the effect of the ZnO on reducing scorch, whilst apparent, is not so pronounced. This observation confirms, in principle, the ability of ZnO to control scorch in SAPA containing rubber formulations. It is considered that stearic acid plays no role in scorch control in this
15 instance.

Table 10 - Zinc oxide as a scorch control additive in NR mixes with SAPA

	Reducing ZnO and Stearic acid (SA) proportions					
	1.5phr SAPA	1.5phr SAPA	1.5phr SAPA	0.5phr SAPA	0.5phr SAPA	0.5phr SAPA
Accelerators CBS/MOR present	SMR20=100phr ZnO=4phr SA=2phr S=2phr CB(FEF) = 51phr	SMR20=100phr ZnO=2phr SA=1phr S=2phr FEF=51phr	SMR20=100phr ZnO=1phr S=2phr FEF=51phr	SMR20=100phr ZnO=4phr SA=2phr S=2phr FEF=51phr	SMR20=100phr ZnO=2phr SA=1phr S=2phr FEF=51phr	SMR20=100phr ZnO=1phr S=2phr FEF=51phr
Cure properties Mooney viscosity ML 1+4 100°C	28	29	33	34	44	51
Mooney Scorch 125°C (minute)	14	12	9	24	16	14
Optimum curing time (t ₉₀) at 160°C (min)	12'40	12'30	9'50	15'30	15'30	14
Physical Properties						
Tensile strength MPa	13.4	15.8	12.6	13	14.3	12
100% modulus MPa	2	1.88	1.76	1.96	2.4	1.6
300% modulus MPa	9.2	9.3	7.7	8.86	10	6.8
Tear strength N/2mm	66	50	42	36	38	37
Elongation at break	375	415	410	385	370	430
Hardness IRHD	52	52	48	51	53	49
Rebound Resilience %	54	50	57	53	55	56

Accelerators CBS and Santocure MOR are present at 0.25/0.25 parts

A Simple Mechanism Proposed to Account for the Multiplicity of Functions of SAPA in Rubber Compounding - Ambient Temperature State

- The surfactant can take the form of a fatty acid salt of N-alkyl propylene diamine (R(NH₂) (CH₂)₃NH₃)²⁺2(R₁COO⁻) where R and R₁ are long chain alkyl groups and R₁ is stearic acid or it can be in the form of an aliphatic diamine as represented by N-tallow-1,3-diamino-propane di-oleate.
- 10 In this form the salt of the diamine functions as an internal processing aid and a filler-rubber surfactant enabling wetting to take place between the rubber (hydrophobic)/filler (hydrophilic) interfaces. On heating to vulcanisation temperature, dissociation takes place forming a secondary amine vulcanisation accelerator R NH₂(CH₂)₃NH₂ and a fatty acid 2 R₁ COOH
- 15 as an internal mould release agent and cure rate controller.

Proposed Mechanism to Account for Increase Scorch Time (Cure Retardation) When Zinc Oxide is used in a SAPA accelerated Rubber Formulation

20

- The surfactant may take the form of the salt of an alkyl propylene diamine, shown as (R NH₂(CH₂)₃NH₃)²⁺2(RCOO)⁻ which on heating in the presence of the zinc oxide (or lead oxide) is represented by (RCOO)₂Zn + H₂O + R NH(CH₂)₃NH₂ where the zinc salt of the fatty acid which acts
- 25 as a retarder (being acidic) to the diamine accelerator produced, and the diamine acts as an accelerator of cure.

Also ZnO is thought to react with H₂S, considered to be produced during all sulphur type cures, hence causing a decrease in the quantity of

30 the hydrogen sulphide normally available and required to produce the nucleophilic hydrosulphide, sulphide, or sulphite ions; these ions are considered essential to effect the hydrolysis of the cyclic S - S chain of



35 sulphur, enabling it to function as a crosslinking agent in rubber. Hence a reduction in their availability due to H₂S reacting with ZnO would account for cure retardation.

Series 7 Experiments. Effect of SAPA on Compression Set (and Cure State)
(Table 11)

- Table 11 and Figure 5 illustrate the effect on compression set of SAPA (3 phr) compared with zero oil and other common rubber mineral based processing oils (7.5p) and mineral oil/processing aid combinations (5p + 5p). It is obvious from these results that the SAPA containing compound reaches a higher state of cure than the non-oil and oil and oil/processing aid formulations as shown by the ODR of Figure 5, and that this observation is confirmed by the lower compression set data for SAPA mixes of Table 11.
- 10 SAPA containing mixes have a compression set value about 12% better (i.e. 25.5%) than the non-oil containing control which has the next best value of 30% compression set. Both SAPA and non-oil formulations are superior to all oil containing formulations.
- 15 A further point of interest is that the density (S.G.) of SAPA mixes was less than that of all other indicating relatively low volume cost potential.

Table 11 - Effect of SAPA on Compression Set (and cure state)

20

Formulation	*Compression Set	Specific Gravity
25 Zero oil i.e. no plasticiser	30	1.1385
7.5 phr Iraqi oil (aromatic oil)	31	1.1328
7.5 phr naphthenic oil. Cirocol 4240 (1)	31	1.1293
7.5 phr Sun oil. Sundex 790 (1) (Aromatic oil)	32	1.1343
30 7.5 phr Dutrex 729 (aromatic oil) (2)	31.5	1.1328
5 phr Iraqi oil + 5 phr Strucktol Sb 212 (3)	32	1.1356
Surface active plasticiser 3phr (+0.5 p ZnO)	25.5	1.1166
Accelerator		

*Compression set was performed at 25% strain and 70°C for 48 hours.

- 35 (1) Trade name of sun Oil Company
 (2) Trade name of Shell
 (3) Trade name of Schill and Seilacker

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Series 8 Experiments. Processing Studies using SAPA (Tables 12-14) (Figure 6)

5 The processing properties of rubber (NR/SBR of table 6) containing SAPA was compared with various aromatic and naphthenic mineral oils, and also with those mixes which contained mineral oils plus the processing aids, stearic acid and Struktol SWb 212. Details of the experimental procedures used and results obtained are given in Tables 12-14 with the exception of the extrusion conditions which are given below.

Table 12 - Internal Mixing Studies of SAPA Compared with Hydrocarbon Mineral Oils and Processing Aids

Mix No.	Formulation	Starting Temp. °C	Dump Temp. °C	Mooney Viscosity (1+4) 100°C	Power Consumption Kw hour	Total Work mJ.m ⁻³	Mixing Cycle Mins.	Ram Pressure kg.cm ⁻²	Fill Factor
1(A)	Zero Oil i.e. No (Plasticiser)	20	135	47	0.535	1533	13 First Stage Only	4.5	0.8
2(A)	7.5 phr Iraqi Oil (Aromatic Oil)	18	119	41	0.38	1089.2	10	4.5	0.8
3(A)	7.5 phr Naphthenic Oil Circosol 4240 (1)	21	117	42	0.3625	1039	10	4.5	0.8
4(A)	7.5 phr Dutrex 729 (Aromatic Oil) (2)	19	115	45	0.3875	1110	10	4.5	0.8
5(A)	7.5 phr Sun Oil Sundex 790 (1) (Aromatic Oil)	20	119	45	0.39	1117	10	4.5	0.8
6(A)	5 phr Iraqi Oil + 5 phr Stearic Acid	18	112	44	0.3575	1024	10	4.5	0.8
7(A)	5 phr Iraqi Oil + 5 phr Strucktol SWB 212 (3)	21	114	48	0.3675	1053	10	4.5	0.8
8(B)	Surface Active Plasticiser Accelerator 3phr (+ 0.5 p ZnO)	20	122	55	0.385	1103	10	4.5	0.8

Scorch Time 27 from 13 (1) Sun Oil Company; (2) Shell; (3) Schill and Schillaker
 Note A laboratory Banbury BR model was used of 1200 ml capacity.

Note A indicates the use of formulation A (conventional organic accelerators present)
 B indicates the use of formulation B (ie no organic accelerators present)

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Table 12 (continued)

<u>Formulation A</u>	<u>Phr</u>
SMR 20	30
SBR 1500	70
ZnO	4
S	2
CBS	0.25
Santocure MOR	0.25
Flectol-H	0.75
IPPD	2
Stearic Acid	2
Wax	3
Plasticiser	as mentioned in the table
FEF	51

** Die Swell : it is calculated by dividing the die swell index by the Specific Gravity of each compound and then dividing the products by 0.5cm^2 which is the cross sectional area of Garvey Die.

Formulation B Plasticiser containing formulations

	<u>Phr</u>	
SMR 20	30	
SBR 1500	70	
ZnO	0.5) used to extend scorch time from 13 mins
S	2) to 27 minutes.
Flectol-H	0.75	
IPPD	2	
Wax	3	anti-ozonant type
Plasticiser	As mentioned in the table	
FEF Black	51	

1. Each compound was passed once through an open mill having a 9 inch diameter and 18 inches length and the nip was kept constant (3mm opening) throughout the passing of each compound.

2. Total Work is calculated as follows:

$$\begin{aligned}
 \text{Total Work is mJ/m}^3 &= \frac{\text{Total energy}}{\text{Fill Factor} \times \text{Banbury chamber volume}} \\
 &= \frac{\text{mJ}}{0.8 \times 1570 \text{ cc}} \\
 &= \frac{\text{mJ}}{1256 \text{ cc}} \\
 &= \frac{\text{mJ}}{1256 \text{ m}^3} \times 10^6
 \end{aligned}$$

Total energy was calculated using a counter which is directly connected to the main power meter of the Banbury, and it was found that each unit is equal to 18 kJ. So for each mix the number of units was counted and accordingly the power was calculated.

Table 13 - Capillary Rheometer Extrusion Studies of SAPA with Hydrocarbon Mineral Oils and Processing Aids

* Extrusion using Davenport Rheometer

Formulation	Flow Rate g/min	Die Swell Ratio	Shear Stress TW
Zero Phr Oil (ie. No Plasticiser)	3.99	1.15	277
7.5 phr Iraqi Oil (Aromatic Oil)	3.99	1.20	243
7.5 phr Naphthentic Oil Circosol 4240 (1)	3.99	1.20	253
7.5 phr Durex 72g (2)	3.99	1.17	260
7.5 phr Sun Oil Sundex 790 (1) (Aromatic Oil)	3.99	1.17	260
5 phr Iraqi Oil + 5 phr Stearic Acid	4	1.20	243
5 phr Iraqi Oil + 5 phr Strucktol SWB 212 (3)	4.06	1.15	278
Surface Active Plasticiser Accelerator 3phr (+0.5 p ZnO)	4.11	1.25	351
(1) Sun Oil Company (2) Shell (3) Schill and Seilacker			

* Flow rate & die swell were calculated at a shear rate of 58.3 sec⁻¹

* The barrel temperature was between 97 - 100°C

* The die used has the following dimensions:

1. length = 15mm
2. diameter = 2 mm

Note

The following equations were the basis for the calculation of the shear rate and the shear stress.

$$\text{Shear rate } \dot{\gamma} \text{ (sec}^{-1}\text{)} = \frac{4Q}{\pi r^3}$$

where Q = volumetric flow rate = output rate
r = radius of die

$$\text{Shear Stress (TW)} = \frac{4Pr}{2L} \quad \text{KN/m}^2$$

ΔP = pressure in barrel
r = radius of die
L = length of die

Table 14 - Extrusion - Processability Evaluation by the use of Garvey Die of SAPA v Oil v Oil/Processing Aid

Formulation*	Flow Rate m/min	Die Swell Index g/cm	**Die Swell Ratio	Head Pressure kN/m ²	Die Temp. of extrudate °C	*** Swelling Edge and Porosity	Formulations Grading	Surface	Corners
Zero Oil (ie No plasticiser)	4.22	0.833	1.463	4343	98	4	3	4	4
7.5 phr Iraqi Oil (Aromatic Oil)	4.24	0.842	1.486	3723	95	4	3	4	4
7.5 phr Naphthenic Oil Circosol 4240 (1)	4.25	0.838	1.484	4033	95	4	3	4	4
7.5 phr Dutrex 729 (Aromatic Oil) (2)	4.30	0.842	1.486	4095	95	4	4	4	4
7.5 phr Sun Oil Sundex 790 (Aromatic Oil) (1)	4.24	0.842	1.484	3909	95	4	4	4	4
5 phr Iraqi Oil + 5phr Stearic Acid	4.24	0.84	1.489	3971	94	4	3	4	4
5 phr Iraqi Oil + 5 phr Strucktol SMB 212 (3)	4.26	0.84	1.479	4288	94	4	4	4	4
*Surface Active Plasticiser Accelerator 3 phr (+0.5 ZnO)	4.31	0.835	1.496	4964	94	4	4	4	4

(1) Sun Oil Company; (2) Shell; (3) Schill and Seilacker Extruder used was a cold feed type of L/D ration 20:1

Extrusion Conditions for SAPA Evaluation

The conditions for extrusion were kept constant throughout the extrusion of the eight compounds and these conditions were as follows:-

1. Temperature of the mill was kept constant at 20°C and the mixing
5 (warming) of the compounds also kept constant, for a period of 4 minutes cutting of the compound was carried out through an interval of 30 seconds.
2. Extruder
10
 - A. - Temperature of the barrel = 70°C
 - B. - Temperature of the head = 110°C
 - C. - Temperature of the die = 110°C
 - D. - Screw Speed = 45 rpm
3. A take off conveyor was kept constant as a speed of 4ft/min to prevent
15 any stretching.

The type of extruder used is 1½" extruder of Farrel-Bridge Ltd which has
20 a length to diameter ratio of 20:1. Formulations used were the same as those given in Table 12 for the mixing study.

Die swell was calculated by dividing the die swell index by the specific gravity of each compound and the results were divided by the cross-sectional area of that of Garvey die which is 0.5 cm².

25

Extrusion Figure 7 also demonstrates use of SAPA as a processing aid in both black and silica filled mixes. It is self-evident that the inclusion of SAPA in the formulation has resulted in a considerable reduction in the otherwise rough surfaces of both of the extrudates. However, SAPA is found
30 particularly effective as a flow additive in the silica filled mix turning on otherwise unprocessable rubber with a compound possessing satisfactory flow. This observation has been found to be generally applicable and SAPA is a particularly effective flow additive for turning "difficult to flow" silica filled rubber mixes into readily processed materials; an additional advantage
35 is that as SAPA, when heated, decomposes and produces in situ a secondary amine then high silica containing formulations can use much lower quantities of accelerators whilst still attaining the same cure state.

Internal Fixing Properties (Table 12)

The mixing parameters of the oil, oil + processing aid, and SAPA rubber mixes were all found to be similar in nature with respect to mixing time, electrical power consumption, and total work input as a result of the mixing operation. However, a special feature observed is that the Mooney viscosity of the SAPA mixes is 8 points greater than the zero oil mixes and 8-14 points greater than the oil and oil/processing aid mixes. This is considered to indicate that as a result of the heat generated in the rubber by mixing, the SAPA is undergoing or promoting a chemical reaction between itself and the rubber mix which results in an increase in Mooney viscosity. It is postulated that the SAPA is, to some extent, functioning as a coupling agent between the filler and the rubber and, or, perhaps as a surfactant between the filler and the rubber. The proposal that SAPA acts as a coupling agent is also based on the observation that all SAPA mixes possess higher modulus values than their oil containing controls (e.g. see Table 7).

As this increase in Mooney viscosity is also observed to occur in unfilled (gum) rubber mixes (see Tables 1(a) & 2) an alternative possibility that must be considered is the reaction of the SAPA directly with the rubber molecule itself to produce in situ a few chemical crosslinks; should such a process occur it would be analogous to the formation of a lightly gelled rubber similar to the SP natural rubber or divinyl benzene SBR series.

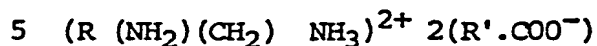
25 Extrusion Processability (Tables 13 and 14 and Figure 6) (graphs A to H) Table 13 gives the extrusion processability measured by capillary rheometer; the results apparently show that the use of SAPA as an alternative to mineral oils for processing purposes give unvulcanised rubber with higher green strength as indicated by an extrusion shear stress of 351 kNm^{-2} for SAPA mixes compared with a range of 243-278 for the more conventional rubber mixes: this confirms the earlier observation of SAPA mixes possessing higher Mooney viscosity which is now reflected in the higher shear stress needed for extrudates.

Table 14 gives Garvey Die data for all SAPA mineral oil, and mineral oil plus processing oil mixes.

All this data confirms the excellent processability of SAPA mixes compared with the conventional rubber formulations demonstrating that no abnormal or adverse processing phenomenon result from the use of SAPA as a rubber compounding ingredient.

Chemical Composition of the Surface Active Plasticiser Accelerator (SAPA) Series

The composition of the SAPA used in this investigation is:-

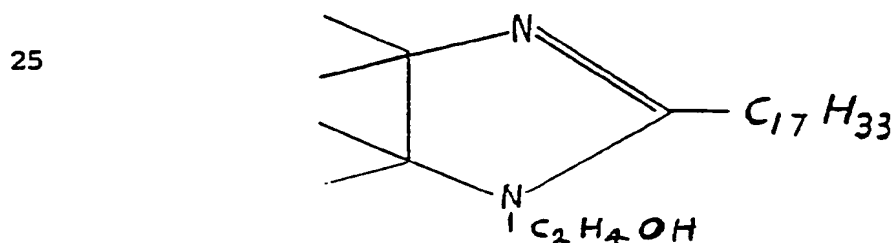


where R= tallow and R'= oleate.

10 This compound has the ability to partially dissociate on heating into some of its primary components and it is this property which is considered to account for its simultaneous multiplicity of uses as a rubber processing aid, cure rate activator and accelerator, and as a surface active plasticiser that enhances filler reinforcement of rubber by means of the mechanism disclosed 15 above.

The fatty acid salt of an alkyl alkylene diamine is selected from the group comprising lauric acid; palmitic acid; soya acid; hydrogenated tallow acid; N-coco-1, 3-diamino-propane; N-tallow-1, 3-diamino-propane N-oleyl-1, 3-diamino-propane; N-tallow-1, 3-diamino-propane di-oleate; N, stearic-1, 3- 20 diamino-propane distearate; N-oleyl-1, 3-diamino-propane dioleate, and alkyl propylene diamine.

Alternatively, the following compositions may be utilised:-



that is:- 1(2-hydroxyethyl)-2-heptadecyl[2] imidazoline or 1 hydroxyethyl 2 oleyl imidazoline.

In yet a further alternative class of cationic surfactants alkyl bis alkylamide may be selected from the group comprising N,N'-ethylene bis 35 lauramide; N,N'-ethylene bis stearamide; N,N'-ethylene bis myristamide; N,N'-ethylene bis oleamide; N,N'-ethylene bis erucamide; and N,N'-ethylene bis behenamide.

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SAPA as a dispersant in Natural Rubber (an example of a strain crystallisable rubber)

SEM micrograph (x 7,000 magnification) of a torn vulcanisate surface to illustrate the ability of the SAPA surfacant as a filler dispersion and wetting agent in Natural Rubber.

(a) contains no SAPA. Figure 8(a)

(b) contains 2 phr of SAPA. Figure 8(b)

10

The micrograph (a) clearly shows lumps of undispersed filler aggregates whilst in (b) the number of undispersed aggregates is considerably reduced. The tensile strength of the SAPA containing mix is ca. 20% greater than its non-SAPA containing comparison.

15

(Formulation: Nr100, FEF Black 50, Aromatic Oil 5, Flectol H 2, CBS 0.5, Suphur 2)

20

SAPA as a filler wetting agent in SBR (an example of a non-strain crystallisable rubber)

SEM micrograph (x7,000 magnification) of a torn SBR vulcanisate surface.

25

(c) contains no SAPA and the relatively poor dispersion of filler aggregates can be seen as represented by large lumps. Figure 9(a)
Tensile strength = 18 MPa, 300% modulus 8 MPa

30 (d) contains SAPA (2 phr) and this has the result of reducing the number of filler aggregates (fewer lumps and voids are visible) and also reducing the relative size of residual aggregates. Tensile strength = 22 MPa. 300% modulus 11 MPa. Figure 9(b)

The better dispersion of the filler through the use of SAPA has increased the tensile strength by 22% and the 300% modulus by 37%.

35

Filler dispersing properties of SAPA

The use of a cationic surfactant as a dispersing and wetting agent for filler in rubber can be seen by inspecting the scanning electron microscopy (SEM) micrographs in Figures 8 and 9. The torn surface of rubber

5 vulcanisates containing no SAPA show relatively large rugosities and voids on their torn surfaces, whilst SAPA containing formulations have almost smooth protrusion and void free surfaces. This is taken to indicate superior aggregate breakdown, filler dispersion and also surface wetting of SAPA containing formulations. Results are shown in Figures 8 and 9. The

10 better filler dispersion has also resulted in higher tensile strength in these particular rubber mixes where filler dispersion was only of average quality. It is speculated that the use of SAPA and similar cationic surfactants in rubber compounding would result in more reproducible rubber mixing operations.

Discussion

It is considered that SAPA has demonstrated multiple functions when used as a rubber compounding additive in various rubbers. In all the classes of rubber examined it functioned as an excellent processing aid or flow additive at low proportions (ca. 0.5 - 2.0 phr). With certain rubbers such as NR, and N/SBR blends in both unfilled and filler reinforced compounds it increases Mooney viscosity and hence green strength; in other rubbers such as SBR, CR and NBR it functions as a flow additive only and does not increase the green strength. SAPA is universal in its effect as a processing flow additive with all common rubbers; it also provides excellent roll release and mould release properties.

Physical properties of vulcanisates of non-polar rubbers such as NR, NR/SBR blends are all increased by the inclusion of SAPA with increases typically between 15-30% of the control mixes based on conventional oils or other flow additives. SAPA is observed to be particularly effective when used in precipitated silica reinforced SBR rubber (see Table 3) where it outperforms TEA.

SAPA also can function as a cure rate promoter; rubber mixes based on the conventional organic accelerator/zinc oxide/stearic and acceleration system can be further accelerated by the inclusion of 0.5 - 2.0 phr of SAPA in the formulation enabling if desired, the proportion of organic accelerator to be reduced. However, it is also observed that for NR, SBR and NR/SBR blends the SAPA will function as an accelerator system in its own right enabling fast curing formulations to be obtained without the presence of any organic accelerator (e.g. CBS/zinc oxide/stearic acid combination (Table 8)). Delayed action curing of SAPA mixes (i.e. longer scorch times) can be obtained by using combinations of SAPA with zinc oxide e.g. 2p of SAPA + 0.5 p ZnO (Table 9).

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It is observed that several types of cationic chemical compounds demonstrate, in principle, multipurpose roles similar to SAPA but with interesting variants. For example, degrees of delayed action cure effects are shown dependent on the particular chemical structure of the
5 surfactant.

It is considered that a new class of rubber compounding ingredient has been identified possessing a multipurpose role by combining into a single chemical structure the functions of internal processing aid and mould
10 release agent, accelerator, and, filler-rubber coupling/wetting agent properties which enhance the strength of rubber vulcanisates.

In addition to enhancing processability of rubber by increasing flow and simultaneoulsy providing mould release and enhancing the properties of the
15 final vulcanisate the cost of a typical SAPA containing rubber formulation is expected to be less than its conventionally accelerated counterpart.

Other properties are also considered to be capable of being improved in
20 rubber formulations by the inclusion of SAPA in the recipe and are identified as follows:

1. Electrical conductivity is increased giving rise to possible advantages in compounds that need to be micro-wave heated more quickly, also by acting as a non-black anti-static agent in rubber
25 compounds.
2. An anti-static agent for non-black (coloured) rubber vulcanisates.
3. Rubber vulcanisates incorporating SAPA have significantly lower coefficient of friction surfaces and may be useful in applications where low surface drag is important.
- 30 4. Reduction in mould fouling - has also been observed, especially with fluoroelastomer rubbers, and also with other elastomers.

CLAIMS:

1. A process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising a fatty acid salt of an alkyl alkylene diamine.
2. A process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising a fatty acid salt of an alkyl alkane diamine.
3. A process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising a fatty acid salt of an alkyl imidazoline.
4. A process as claimed in claim 3, characterised in that the fatty acid salt of an alkyl imidazoline is selected from one of 1(2-hydroxyethyl)-2-heptadecenyl [2] imidazoline and 1 hydroxyethyl 2 oleyl imidazoline.
5. The use of a cationic surfactant comprising a fatty acid salt of an alkyl alkylene diamine in the treatment of rubber wherein the cationic surfactant is mixed with the rubber to provide a rubber compound with improved flow characteristics and release properties.
6. The use of a cationic surfactant comprising a fatty acid salt of an alkyl alkane diamine in the treatment of rubber wherein the cationic surfactant is mixed with the rubber to provide a rubber compound with improved flow characteristics and release properties.
7. A process of treating a rubber to produce a rubber compound having improved flow characteristics and release properties, comprising taking a rubber and mixing the rubber with a cationic surfactant comprising an alkyl bis alkylamide.
8. The use of a cationic surfactant comprising an alkyl bis alkylamide in the treatment of rubber wherein the cationic surfactant is mixed with the rubber to provide a rubber compound with improved flow characteristics and release properties.

9. A process as claimed in claim 1 or claim 2, characterised in that the fatty acid salt is used in the presence of a metal oxide retardant.
10. A process as claimed in claim 3 or 4, characterised in that the fatty acid salt of an alkyl imidazoline is used in the presence of a metal oxide retardant.
- 5 11. A process as claimed in claim 9 or 10, characterised in that the metal oxide retardant is selected from the group comprising zinc oxide and lead oxide.
12. A process as claimed in claim 1 or claim 2, characterised in that the
10 fatty acid salt is selected from the group comprising lauric acid; palmitic acid; soya acid; hydrogenated tallow acid; N-coco-1, 3-diamino-propane; N-tallow-1, 3-diamino-propane; N-oleyl-1, 3-diamino-propane; N-tallow-1, 3-diamino-propane di-oleate; N, stearic-1, 3-diamino-propane distearate; N-oleyl-1, 3-diamino-propane dioleate, and alkyl propylene diamine.
- 15 13. A process as claimed in claim 7, characterised in that alkyl bis alkylamide is selected from the group comprising N,N'-ethylene bis lauramide; N,N'-ethylene bis stearamide; N,N'-ethylene bis myristamide; N,N'-ethylene bis oleamide; N,N'-ethylene bis erucamide; and N,N'-ethylene bis behenamide.
14. The use as claimed in claim 5 or 8, characterised by the use of the
20 cationic surfactant as a dispersing and wetting agent for filler in rubber.
15. A process as claimed in any one of claims 1 to 4, 7, and 9 to 14, characterised in that the mixture of rubber and cationic surfactant is vulcanised by heating in the presence of sulphur or a sulphur donating compound.
- 25 16. A rubber compound prepared in accordance with the process claimed in any one of claims 1 to 4, 7, and 9 to 14.

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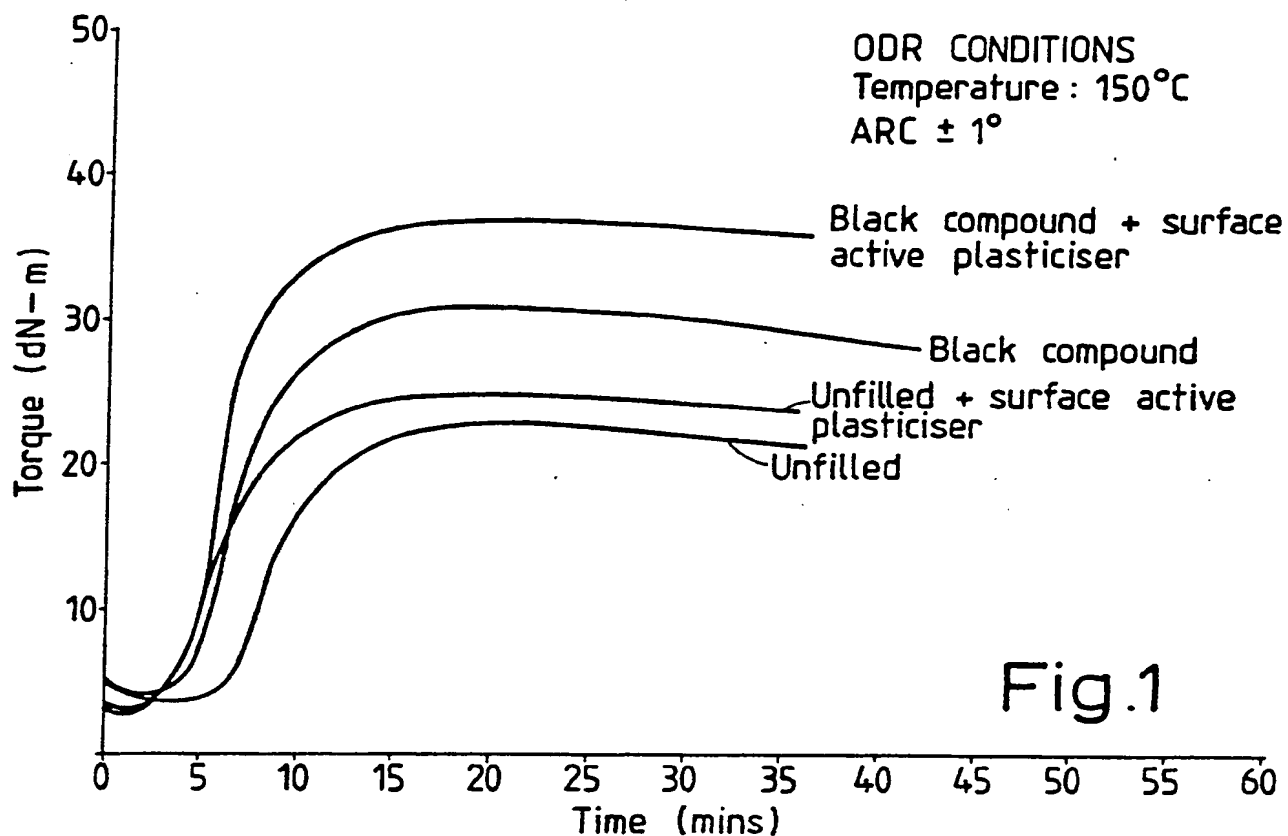


Fig.1

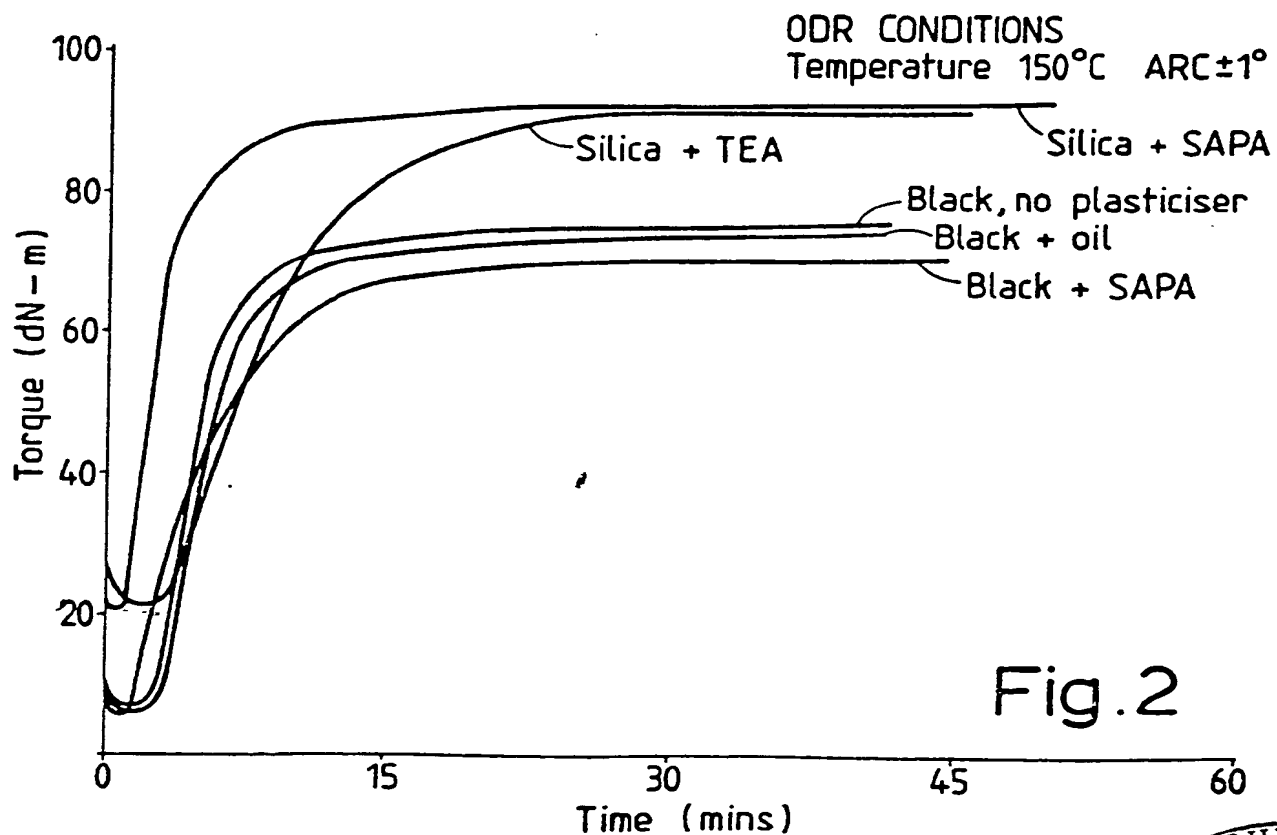


Fig.2

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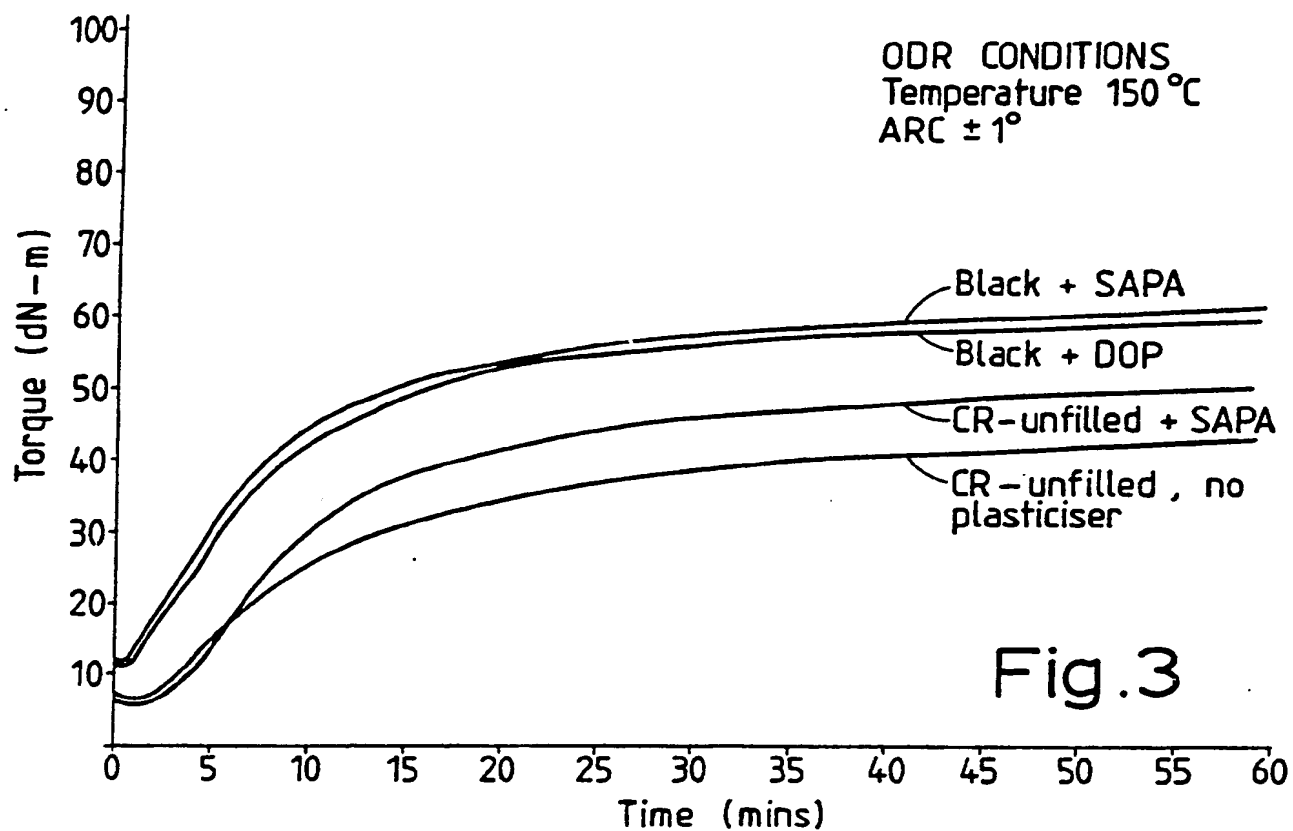


Fig.3

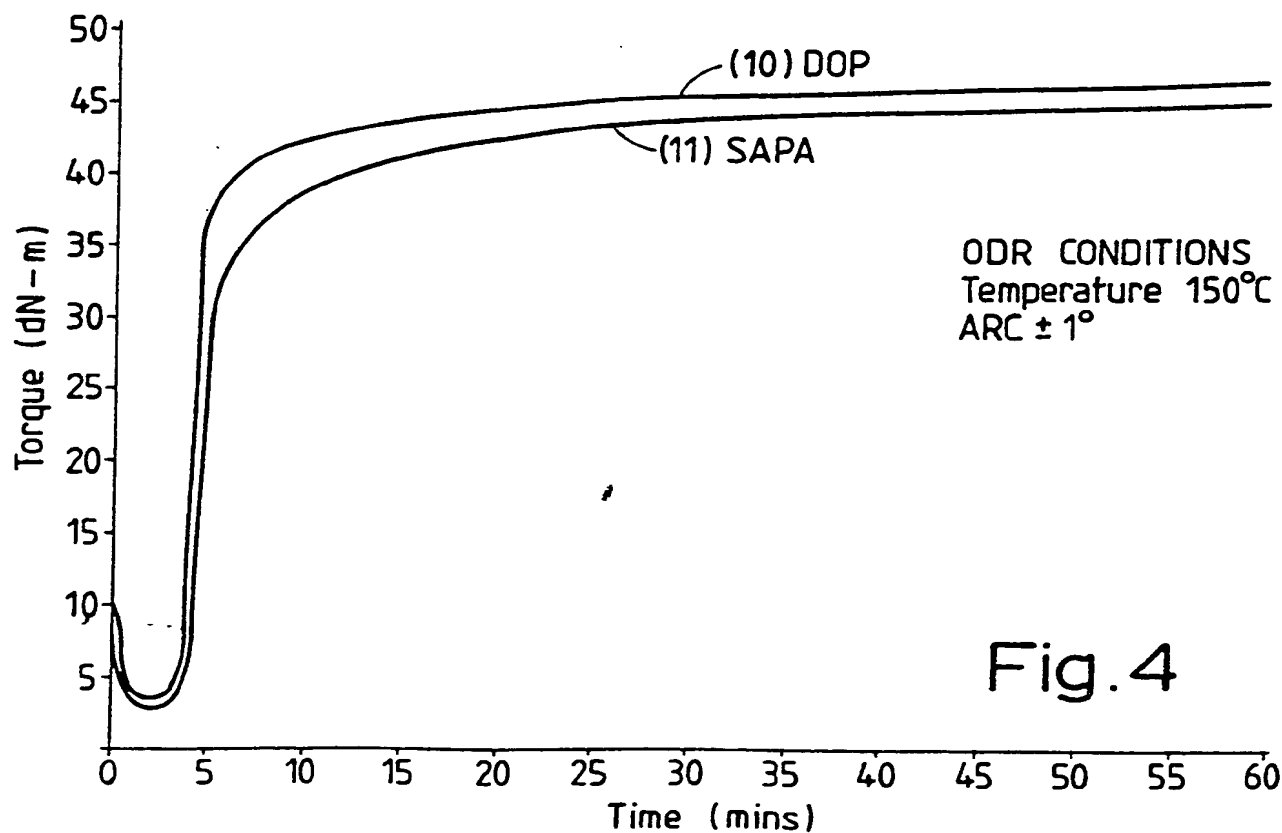


Fig.4

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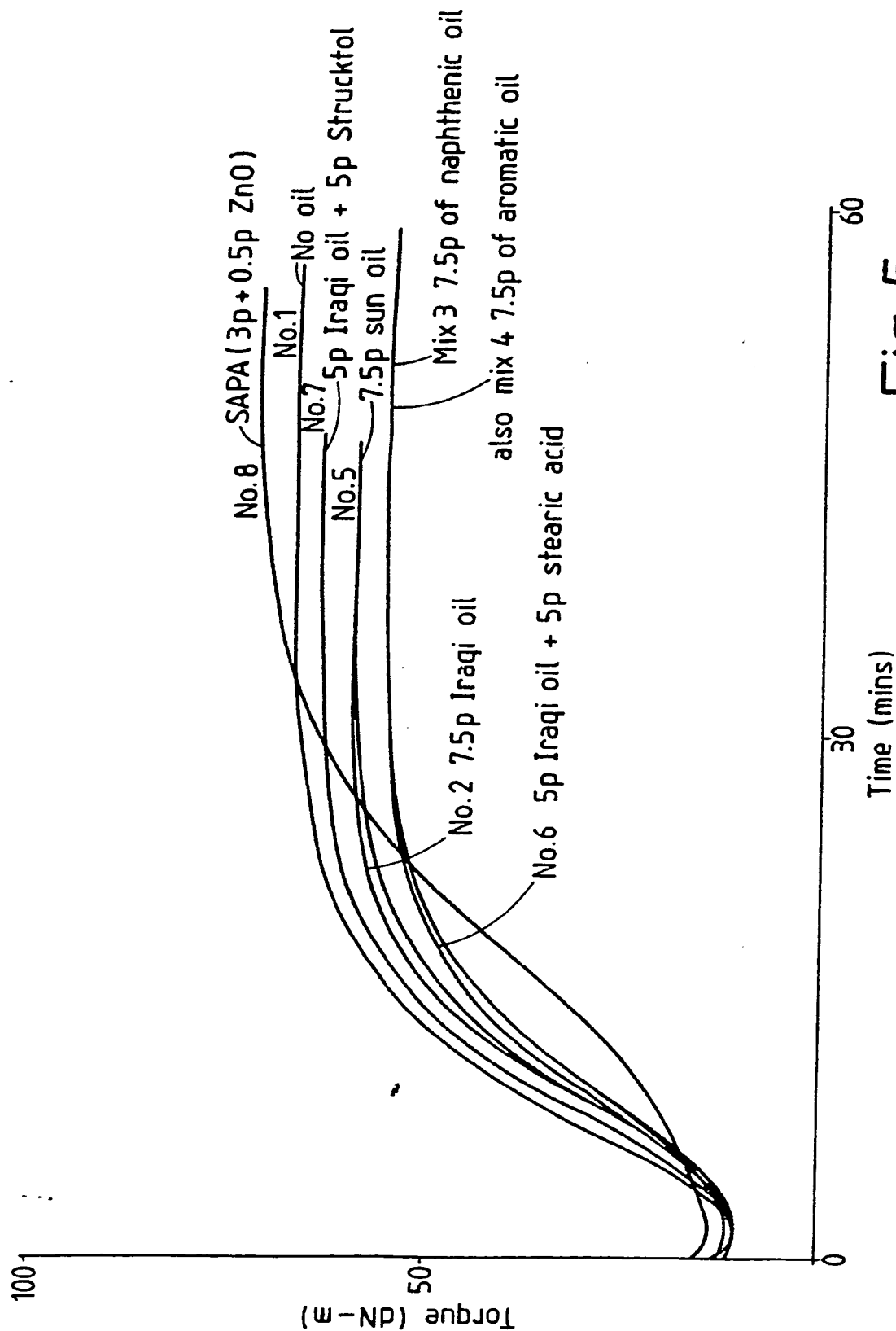


Fig.5

Time (mins)

60

30

0

Torque (dN-m)

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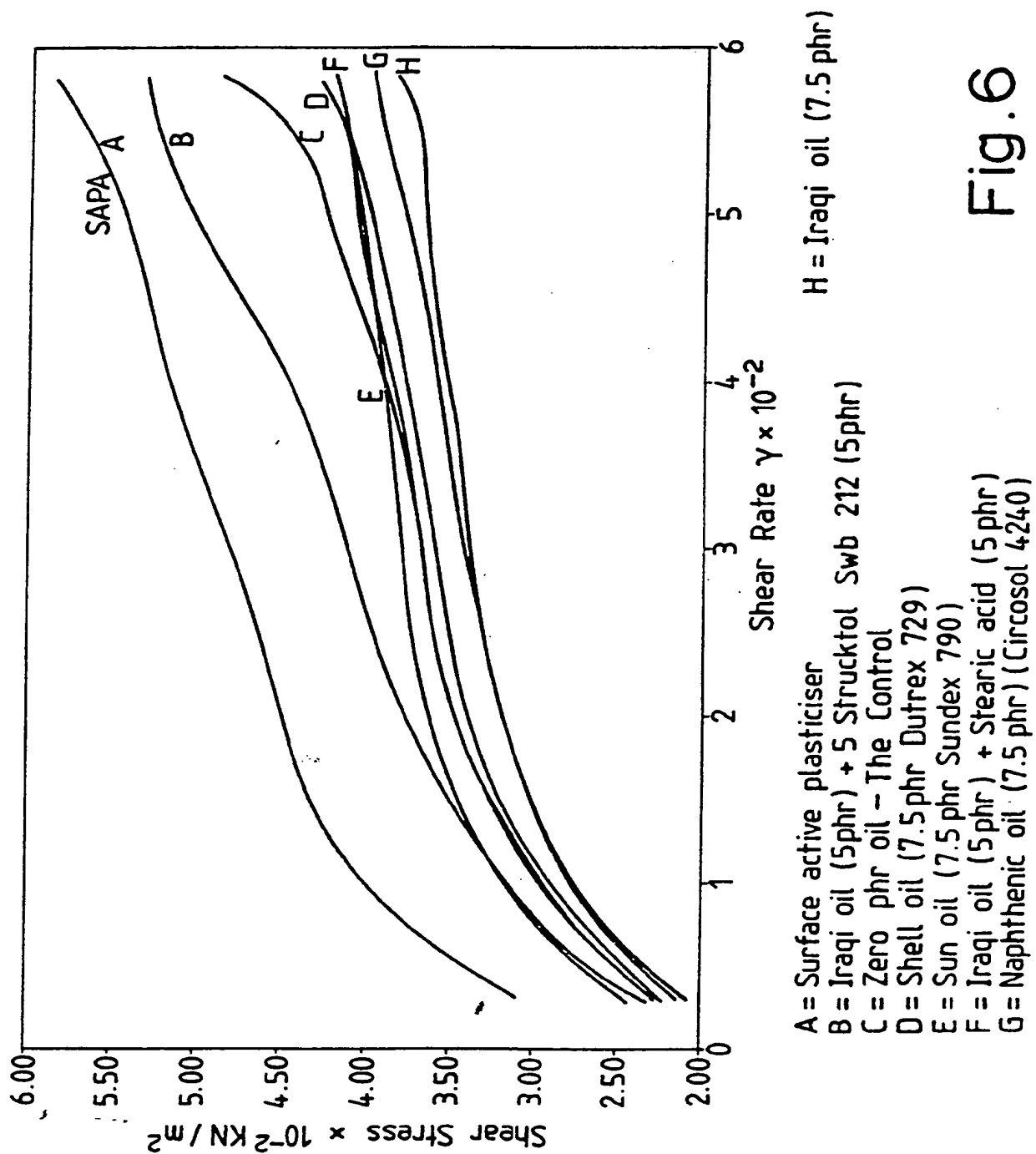


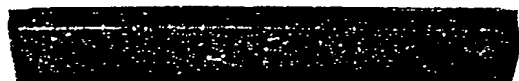
Fig. 6

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No SAPA

Fig. 7a



2phr SAPA

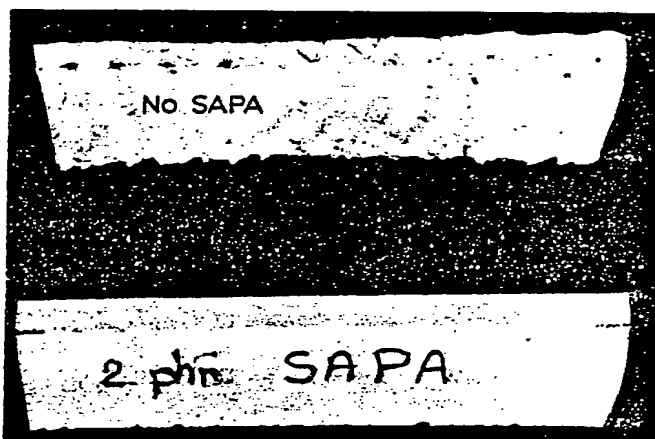
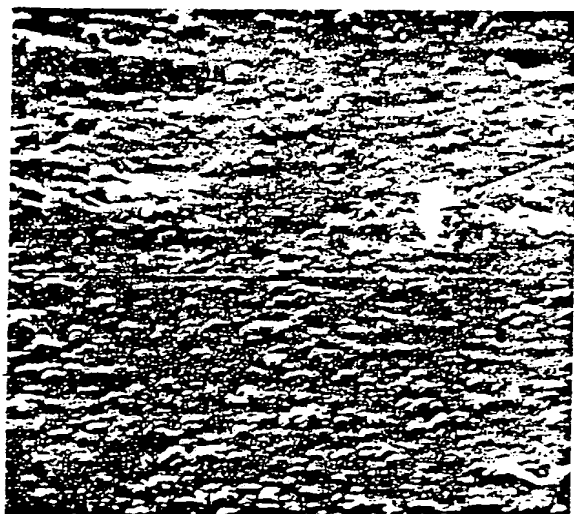


Fig. 7b



Undispersed large aggregate

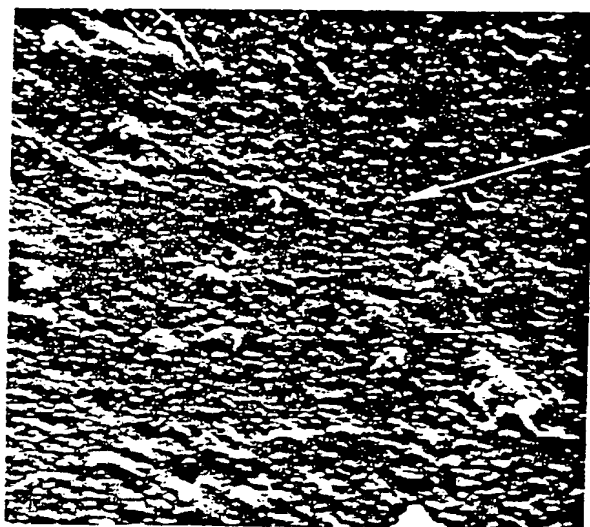
Fig. 8a

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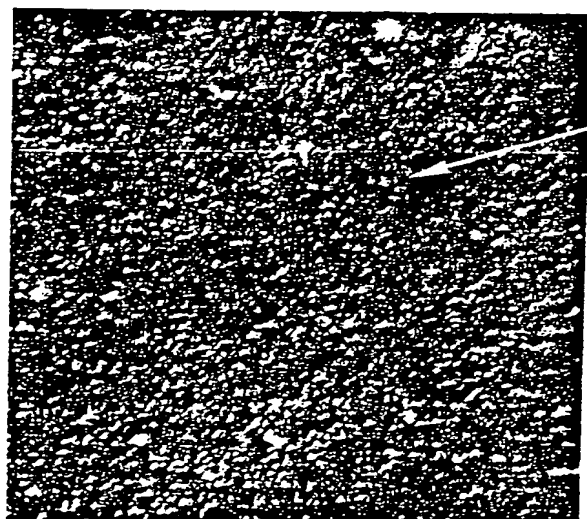
Undispersed small
aggregate

Fig. 8b



Undispersed large
aggregate

Fig. 9a



Undispersed small
aggregate

Fig. 9b

INTERNATIONAL SEARCH REPORT

International Application No PCT/GB 84/00168

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC ³ : C 08 L 21/00; C 08 K 5/17; C 08 K 5/20; C 08 K 5/34		
II. FIELDS SEARCHED		
Minimum Documentation Searched *		
Classification System	Classification Symbols	
IPC ³	C 08 L; C 08 K	
Documentation Searched other than Minimum Documentation to the extent that such Documents are Included In the Fields Searched *		
III. DOCUMENTS CONSIDERED TO BE RELEVANT ¹⁴		
Category *	Citation of Document, ¹⁴ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No. ¹⁴
X	EP, A, 0076197 (RHONE-POULENC) 6 April 1983, see claims 1,2; page 2, line 38 Chemical Abstracts, volume 73, no. 26, issued 1970, December 28 (Columbus, Ohio, U.S.A.) Luzan V.I. et al.: "Vulcanization of natural rubber in the presence of ethylenediamine and its derivatives" see page 34, abstract 131774k, Khim.Prom.Ukr.1970, (4), 17-19 (Russ).	7,8,13-16
X	EP, A, 0005617 (JAPAN SYNTHETIC RUBBER) 28 November 1979, see claim 3; page 4, lines 34,35; page 10, table 2	7,8,13-16
Y	US, A, 3502612 (E.J. LATOS) 24 March 1970, see claim 1	1,2,5,6,9, 11,12,14- 16
<p>* Special categories of cited documents: ¹⁵</p> <ul style="list-style-type: none"> "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve ... inventive step "Y" document of particular relevance; the claimed invention cannot ... be considered to involve an inventive step when the document is combined with one or more other such documents, each combination being obvious to a person skilled in the art. "&" document member of the same patent family 		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search :	Date of Mailing of this International Search Report :	
10th August 1984	13.09.84	
International Searching Authority :	Signature of Authorized Officer : ²⁰	
EUROPEAN PATENT OFFICE	G.L.M. Meydenberg	

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, ¹⁶ with indication, where appropriate, of the relevant passages ¹⁷	Relevant to Claim No ¹⁸
A	US, A, 3369004 (L.E. STANTON) 13 February 1968, see claim 4 --	4
A	GB, A, 965203 (SHELL) 29 July 1964, see claim 1 -----	

ANNEX TO THE INTERNATIONAL SEARCH REPORT

INTERNATIONAL APPLICATION NO. PCT/GB 84/00168 (SA 7179)

This Annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 06/09/84

The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A- 0076197	06/04/83	FR-A,B 2513645 JP-A- 58125731	01/04/83 26/07/83
EP-A- 0005617	28/11/79	JP-A- 54148043 US-A- 4281085 US-A- 4371668 JP-A- 55108418	19/11/79 28/07/81 01/02/83 20/08/80
US-A- 3502612	24/03/70	None	
US-A- 3369004		None	
GB-A- 965203		None	